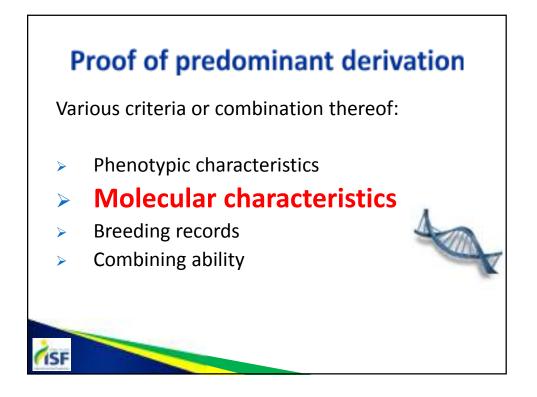
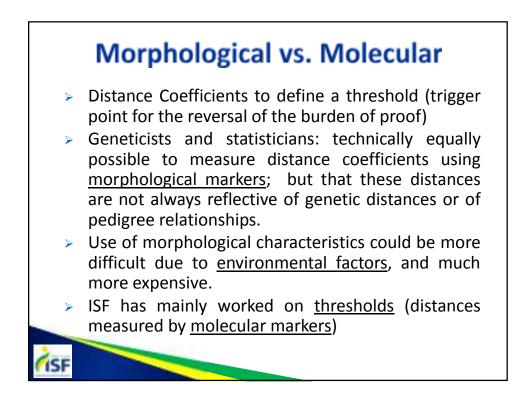


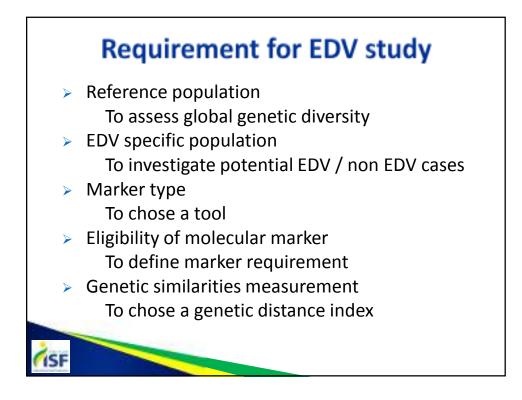
## The ISF approach and a case study to help determine EDV status

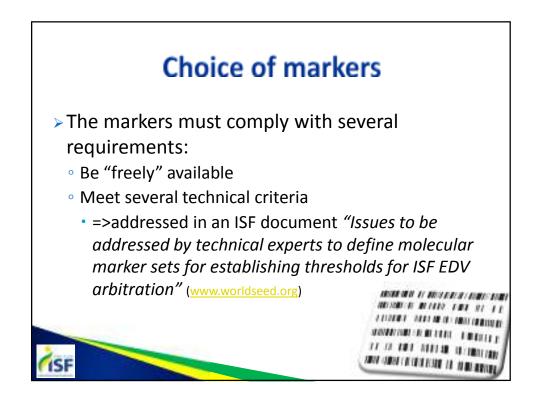
Oct. 2013 International Seed Federation

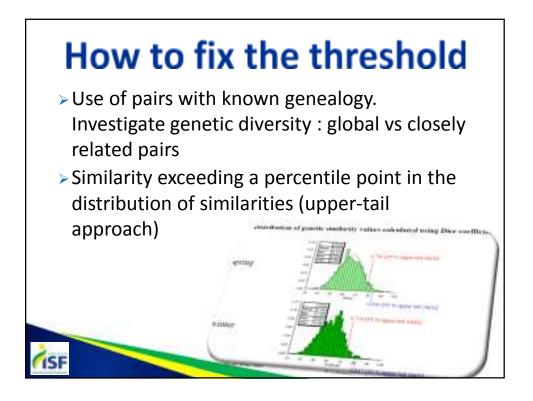


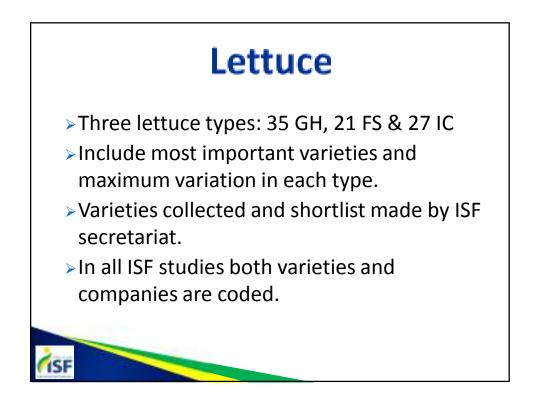


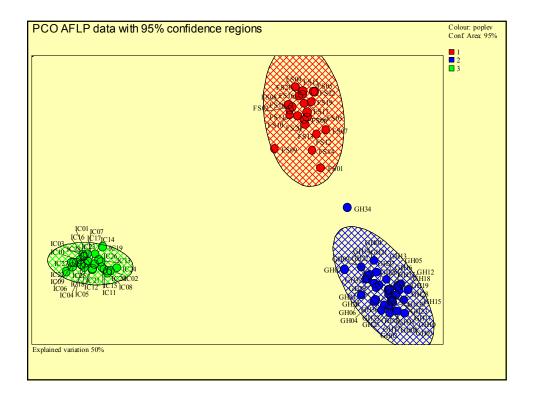




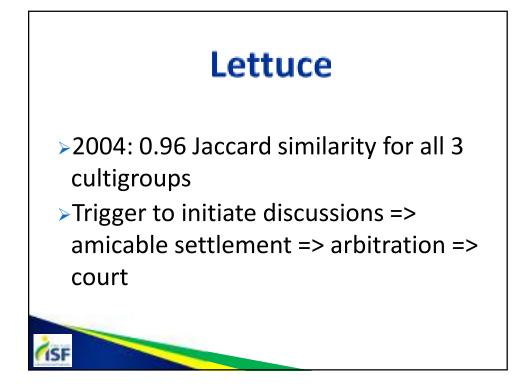


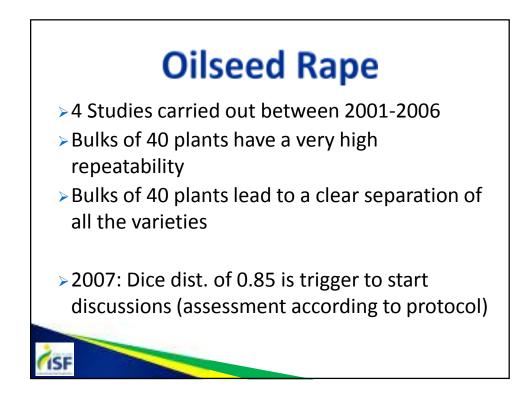


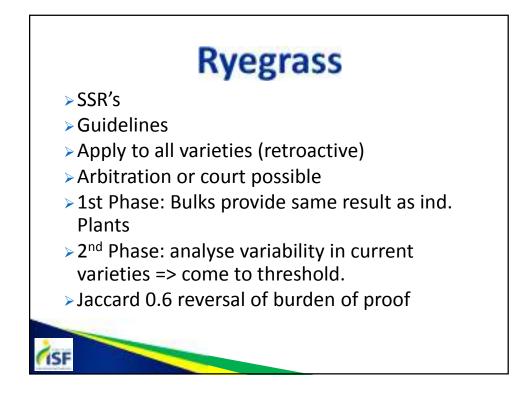


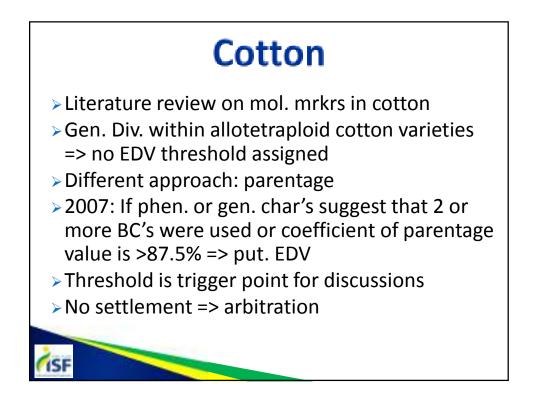


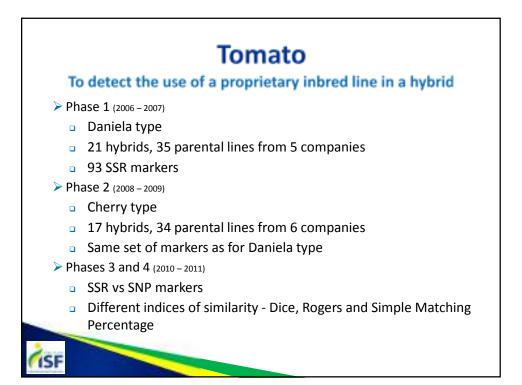
2       0.9990       22       21       5       5       0.9985       0.0028         2       0.9973       19       15       4       4       0.9878       0.0073         2       0.9939       13       11       3       0.9868       0.0073         2       0.9939       13       11       3       0.9816       0.0093         2       0.9930       13       8       3       0.9816       0.0093         2       0.9906       35       30       6       6       0.9740       0.0159         2       0.9852       12       8       3       3       0.9790       0.0132         2       0.9835       11       0.3       0.9666       0.0154       0.0154         2       0.9835       11       0.3       0.9667       0.0141         2       0.9774       30       16       6       0.9691       0.0168         2       0.9774       20       16       4       4       0.9693       0.0169         2       0.9670       12       13       3       0.9682       0.1616         2       0.9677       13       10       3	zone	q	genox g	genoy	Jompx	compy	ali	enomargin	
<ul> <li>GH, Jaccard</li> <li>GH2 and GH22 were selected in the same F3</li> <li>O.973</li> <li>O.973</li> <li>O.976</li> <li>O.976</li> <li>O.977</li> <li>O.978</li> <li>O.977</li> <li>O.978</li> <li>O.978</li> <li>O.977</li> <li>O.978</li> <li>O.977</li> <li>O.978</li> <li>O.9798</li> <li>O.</li></ul>	2						0.9985		
GH, JacCard GH, Ja	2	0.9973	19	15	4	4	0.9878	0.0079	
2       0.9926       35       30       6       6       0.9740       0.0135         2       0.9869       13       8       3       3       0.9710       0.0132         2       0.9869       13       8       3       3       0.9710       0.0132         2       0.9855       12       8       3       3       0.9664       0.0120         2       0.9863       11       10       3       3       0.9664       0.0128         2       0.9805       35       31       6       6       0.9669       0.01017         2       0.9728       12       2       3       1       0.9667       0.0141         2       0.9778       13       30       6       6       0.9651       0.0177         2       0.9774       20       16       4       0.9619       0.0142         2       0.9704       20       16       4       0.9619       0.0164         2       0.9667       16       14       4       0.9619       0.0164         2       0.9664       35       33       6       6       0.9533       0.0166         2 <th>2</th> <th>0.9956</th> <th>11</th> <th>8</th> <th>3</th> <th>3</th> <th>0.9850</th> <th>0.0073</th> <th></th>	2	0.9956	11	8	3	3	0.9850	0.0073	
2       0.9926       35       30       6       6       0.9740       0.0135         2       0.9869       13       8       3       3       0.9710       0.0132         2       0.9869       13       8       3       3       0.9710       0.0132         2       0.9855       12       8       3       3       0.9664       0.0120         2       0.9863       11       10       3       3       0.9664       0.0128         2       0.9805       35       31       6       6       0.9669       0.01017         2       0.9728       12       2       3       1       0.9667       0.0141         2       0.9778       13       30       6       6       0.9651       0.0177         2       0.9774       20       16       4       0.9619       0.0142         2       0.9704       20       16       4       0.9619       0.0164         2       0.9667       16       14       4       0.9619       0.0164         2       0.9664       35       33       6       6       0.9533       0.0166         2 <th>2</th> <th>0.9939</th> <th>13</th> <th>11</th> <th>3</th> <th>3</th> <th>0.9816</th> <th>0.0093</th> <th>GH. Jaccard</th>	2	0.9939	13	11	3	3	0.9816	0.0093	GH. Jaccard
2       0.9889       13       8       3       3       0.9717       0.0135         2       0.9855       12       8       3       0.9702       0.0132         2       0.9838       11       10       3       0.9664       0.0120         2       0.9838       11       10       3       0.9664       0.0120         2       0.9838       12       2       3       1       0.9667       0.0141         2       0.9774       31       30       6       6       0.9667       0.0141         2       0.9778       12       2       3       1       0.9667       0.0141         2       0.9774       13       30       6       6       0.9651       0.0172         2       0.9774       12       10       3       0.9650       0.0188       0.0142         2       0.9771       12       11       3       0.9618       0.0124       0.0124         2       0.9677       12       11       3       0.9618       0.0124         2       0.9677       12       11       3       0.9653       0.0164         2       0.9664	2	0.9922	10	8	3	3	0.9759	0.0095	
2       0.9872       27       25       5       5       0.9702       0.0132         2       0.9855       12       8       3       0.9686       0.0154         2       0.9822       18       16       4       4       0.9671       0.0128         2       0.9802       18       16       4       4       0.9671       0.0128         2       0.9808       112       2       3       1       0.9664       0.0107         2       0.9774       30       18       6       4       0.9661       0.0117         2       0.9774       30       18       6       4       0.9661       0.0138         2       0.9774       12       10       3       0.9663       0.0142         2       0.9774       12       10       3       0.9663       0.0142         2       0.9670       12       11       3       0.9619       0.0124         2       0.9654       35       18       6       4       0.9583       0.0166         2       0.9653       31       16       6       0.9579       0.0154         2       0.9563 <t< th=""><th>2</th><th>0.9906</th><th>35</th><th>30</th><th>6</th><th>6</th><th>0.9740</th><th>0.0159</th><th></th></t<>	2	0.9906	35	30	6	6	0.9740	0.0159	
<ul> <li>2 0.9855 12 8 3 3 0.9686 0.0154</li> <li>2 0.9825 12 8 16 4 4 0.9671 0.0128</li> <li>2 0.9805 35 31 6 6 0.9661 0.0109</li> <li>2 0.9774 31 30 6 6 0.9667 0.0141</li> <li>2 0.9774 30 18 6 4 0.9661 0.0138</li> <li>2 0.9738 13 12 3 3 0.9650 0.0158</li> <li>2 0.9704 20 16 4 4 0.9618 0.0124</li> <li>2 0.9687 16 14 4 4 0.9618 0.0124</li> <li>2 0.9687 16 14 4 4 0.9618 0.0124</li> <li>2 0.9663 1 10 3 3 0.9650 0.0169</li> <li>2 0.9667 0.12 11 3 3 0.9658 0.0169</li> <li>2 0.9637 8 2 3 1 0.9567 0.0169</li> <li>2 0.9654 35 18 6 4 0.9570 0.0159</li> <li>2 0.9566 27 24 5 5 0.9553 0.0164</li> <li>2 0.9550 217 15 4 4 0.9538 0.0165</li> <li>2 0.9550 217 15 4 4 0.9538 0.0165</li> <li>2 0.9502 17 15 4 4 0.9538 0.0165</li> <li>2 0.9409 33 31 6 6 6 0.9579 0.0154</li> <li>3 0.9409 33 31 6 6 4 0.9507 0.0181</li> <li>3 0.9418 12 3 3 1 0.9507 0.0181</li> <li>3 0.9418 12 3</li></ul>	2	0.9889	13	8	3	3	0.9717	0.0135	
<ul> <li>2 0.9855 12 8 3 3 0.9686 0.0154</li> <li>2 0.9825 12 8 16 4 4 0.9671 0.0128</li> <li>2 0.9805 35 31 6 6 0.9661 0.0109</li> <li>2 0.9774 31 30 6 6 0.9667 0.0141</li> <li>2 0.9774 30 18 6 4 0.9661 0.0138</li> <li>2 0.9738 13 12 3 3 0.9650 0.0158</li> <li>2 0.9704 20 16 4 4 0.9618 0.0124</li> <li>2 0.9687 16 14 4 4 0.9618 0.0124</li> <li>2 0.9687 16 14 4 4 0.9618 0.0124</li> <li>2 0.9663 1 10 3 3 0.9650 0.0169</li> <li>2 0.9667 0.12 11 3 3 0.9658 0.0169</li> <li>2 0.9637 8 2 3 1 0.9567 0.0169</li> <li>2 0.9654 35 18 6 4 0.9570 0.0159</li> <li>2 0.9566 27 24 5 5 0.9553 0.0164</li> <li>2 0.9550 217 15 4 4 0.9538 0.0165</li> <li>2 0.9550 217 15 4 4 0.9538 0.0165</li> <li>2 0.9502 17 15 4 4 0.9538 0.0165</li> <li>2 0.9409 33 31 6 6 6 0.9579 0.0154</li> <li>3 0.9409 33 31 6 6 4 0.9507 0.0181</li> <li>3 0.9418 12 3 3 1 0.9507 0.0181</li> <li>3 0.9418 12 3</li></ul>	2	0.9872	27	25	5	5	0.9702	0.0132	GH21 and GH22 were
2       0.9822       18       16       4       4       0.9671       0.0128         2       0.9805       35       31       6       6       0.9669       0.0107         2       0.9788       12       2       3       1       0.9667       0.01017         2       0.9774       30       18       6       4       0.9661       0.0138         2       0.9738       13       12       3       3       0.9660       0.0141         2       0.9774       20       16       4       4       0.9619       0.0124         2       0.9704       20       16       4       4       0.9619       0.0124         2       0.9664       35       18       6       4       0.9593       0.0169         2       0.9664       35       18       6       4       0.9583       0.0169         2       0.9653       31       16       6       0.9579       0.0154         2       0.9563       31       16       6       0.9579       0.0154         2       0.9553       31       16       6       0.9574       0.0169         2<	2	0.9855	12	8	3	3	0.9686	0.0154	OTIZI UTU OTIZZ WETC
2       0.3922       10       10       4       4       0.3011       0.0110         2       0.9805       33       6       6       0.9667       0.0101         2       0.9788       12       2       3       1       0.9667       0.0101         2       0.9774       30       18       6       4       0.9661       0.0108         2       0.9738       13       12       3       3       0.9660       0.0188         2       0.9738       13       12       3       3       0.9663       0.0141         2       0.9704       16       4       4       0.9619       0.0108         2       0.9670       12       11       3       0.9612       0.0129         2       0.9620       13       10       3       3       0.9580       0.0169         2       0.9620       13       10       3       3       0.9580       0.0169         2       0.9650       33       16       6       0.9570       0.0154         2       0.9550       33       16       6       0.9570       0.0154         2       0.9553	2	0.9838	11	10	3	3	0.9684	0.0120	colocted in the came
2       0.9788       12       2       3       1       0.9667       0.0141         2       0.9778       13       13       0       6       6       0.9651       0.0103         2       0.9738       13       12       3       3       0.9661       0.0118         2       0.9738       11       12       3       3       0.9661       0.0118         2       0.9738       12       12       3       3       0.9663       0.0142         2       0.9704       10       4       4       0.9619       0.0108       0.0142         2       0.9670       12       11       3       3       0.9612       0.0129         2       0.9667       13       10       3       3       0.9682       0.0160         2       0.9663       33       16       6       4       0.9570       0.0154         2       0.9650       13       10       3       3       0.9562       0.0169         2       0.9653       31       16       6       4       0.9553       0.0154         2       0.9553       31       16       6       0.9553	2	0.9822	18	16	4	4	0.9671	0.0128	Selected III the Same
2       0.9771       31       30       6       6       0.9661       0.0107         2       0.9774       30       18       6       4       0.9661       0.0136         2       0.9738       13       12       3       3       0.9660       0.0142         2       0.9774       20       16       4       4       0.9619       0.0124         2       0.9670       12       11       3       3       0.9612       0.0124         2       0.9674       12       11       3       3       0.9612       0.0124         2       0.9664       35       18       6       4       0.9593       0.0169         2       0.9654       35       18       6       4       0.9583       0.0169         2       0.9603       33       18       6       4       0.9570       0.0164         2       0.9553       31       16       6       0.9570       0.0164         2       0.9553       31       16       6       0.9574       0.0164         2       0.9552       17       16       4       0.9584       0.0201         1<	2	0.9805	35	31	6	6	0.9669	0.0109	
2       0.9754       30       18       6       4       0.9651       0.0138         2       0.9738       13       12       3       3       0.9650       0.0142         2       0.9704       10       3       3       0.9639       0.0142         2       0.9704       12       11       3       3       0.9619       0.0124         2       0.9667       16       14       4       0.9618       0.0124       0.0124         2       0.9667       16       14       4       0.9612       0.0124       0.0124         2       0.9667       16       14       4       0.9612       0.0124       0.0124         2       0.9667       18       6       4       0.9580       0.0166       0.0166         2       0.9637       8       2       3       1       0.9580       0.0164         2       0.9633       31       16       6       4       0.9570       0.0154         2       0.9550       17       15       4       4       0.9530       0.0165         2       0.9502       17       15       4       0.9530       0.0164 <th>2</th> <th>0.9788</th> <th>12</th> <th>2</th> <th>3</th> <th>1</th> <th>0.9667</th> <th>0.0141</th> <th>F4</th>	2	0.9788	12	2	3	1	0.9667	0.0141	F4
2       0.9738       13       12       3       3       0.9650       0.0158         2       0.9704       20       16       4       4       0.9639       0.0142         2       0.9704       20       16       4       4       0.9619       0.0108         2       0.9670       12       11       3       3       0.9612       0.0124         2       0.9657       12       11       3       3       0.9612       0.0129         2       0.9657       12       11       3       3       0.9612       0.0129         2       0.9650       13       10       3       3       0.9582       0.0160         2       0.9620       13       10       3       3       0.9582       0.0160         2       0.9650       33       16       6       4       0.9570       0.0154         2       0.9553       31       16       6       4       0.9536       0.0166         2       0.9553       31       16       6       0.9534       0.0201         1       0.9456       33       16       6       0.9534       0.0201	2	0.9771	31	30	6	6	0.9651	0.0107	
2       0.9721       12       10       3       3       0.9639       0.0142         2       0.9704       20       16       4       4       0.9619       0.0142         2       0.9677       16       14       4       0.9618       0.0124         2       0.9677       12       11       3       3       0.9612       0.0124         2       0.9677       12       11       3       3       0.9612       0.0124         2       0.9664       35       18       6       4       0.9583       0.0160         2       0.9620       13       10       3       0.9652       0.0160         2       0.9653       33       16       6       0.9570       0.0154         2       0.9553       31       16       6       0.9570       0.0154         2       0.9553       31       16       6       0.9574       0.0201         1       0.9456       10       2       3       1       0.9534       0.0201         1       0.9452       33       16       6       0.9511       0.02021       0.0162         1       0.9452	2	0.9754	30	18	6	4	0.9651	0.0138	
2       0.9704       12       10       3       3       0.9639       0.0108         2       0.9670       12       11       3       3       0.9619       0.0108         2       0.9667       16       14       4       4       0.9619       0.0108         2       0.9667       12       11       3       3       0.9612       0.0124         2       0.9667       12       11       3       3       0.9612       0.0129         2       0.9667       8       2       3       1       0.9580       0.0160         2       0.9620       13       10       3       3       0.9582       0.0160         2       0.9620       13       10       3       3       0.9582       0.0160         2       0.9570       30       14       6       4       0.9570       0.0154         2       0.9570       30       14       6       4       0.9536       0.0165         2       0.9502       17       15       4       4       0.9536       0.0165         2       0.9502       17       15       4       4       0.9536	2	0.9738	13	12	3	3	0.9650	0.0158	GH8 and GH11 come
2       0.9687       16       14       4       4       0.9678       0.0124         2       0.9670       12       11       3       3       0.9612       0.0129         2       0.9657       35       18       6       4       0.9593       0.0169         2       0.9657       12       11       3       3       0.9612       0.0124         2       0.9657       12       11       3       3       0.9612       0.0129         2       0.9620       13       10       3       3       0.9582       0.0160         2       0.9620       13       10       3       3       0.9582       0.0164         2       0.9560       33       16       6       4       0.9570       0.0154         2       0.9570       30       14       6       4       0.9553       0.0154         2       0.9562       17       15       4       4       0.9538       0.0165         2       0.9502       17       15       4       4       0.9538       0.0164         1       0.9452       33       16       6       0.9519       0.0201 <th>2</th> <th>0.9721</th> <th>12</th> <th>10</th> <th>3</th> <th>3</th> <th>0.9639</th> <th>0.0142</th> <th></th>	2	0.9721	12	10	3	3	0.9639	0.0142	
2       0.9670       12       11       3       3       0.9612       0.0129         2       0.9654       35       18       6       4       0.9593       0.0160         2       0.9620       13       10       3       3       0.9580       0.0160         2       0.9603       33       18       6       4       0.9580       0.0160         2       0.9603       33       18       6       4       0.9580       0.0160         2       0.9563       31       16       6       4       0.9570       0.0154         2       0.9553       31       16       6       4       0.9563       0.0156         2       0.9553       31       16       6       4       0.9563       0.0154         2       0.9553       31       16       6       4       0.9563       0.0165         2       0.9502       17       15       4       4       0.9534       0.0201         1       0.9452       33       16       6       0.9519       0.0152         1       0.9452       33       16       6       0.9510       0.0201	2	0.9704	20	16	4	4	0.9619	0.0108	from como F2
2       0.9654       35       18       6       4       0.9593       0.0169         2       0.9637       8       2       3       1       0.9587       0.0169         2       0.9637       8       2       3       1       0.9587       0.0160         2       0.9603       33       18       6       4       0.9587       0.0160         2       0.9603       33       18       6       4       0.9580       0.0160         2       0.9656       35       33       6       6       0.9570       0.0154         2       0.9556       31       16       6       4       0.9565       0.0099         2       0.9550       27       24       5       5       0.9553       0.0154         2       0.9519       20       14       4       0.9538       0.0165         2       0.9519       20       14       4       0.9538       0.0201         1       0.9469       33       31       6       6       0.9524       0.0201         1       0.9452       33       33       6       6       0.9519       0.0201	2	0.9687	16	14	4	4	0.9618	0.0124	ITOITI Saitte F3
2       0.9637       8       2       3       1       0.9587       0.0160         2       0.9603       33       18       6       4       0.9580       0.0196         2       0.9603       33       18       6       4       0.9580       0.0196         2       0.9586       35       36       6       0.9570       0.0154         2       0.9570       30       14       6       4       0.9570       0.0154         2       0.9556       31       16       6       4       0.9553       0.0164         2       0.9550       27       24       5       5       0.0154         2       0.9550       27       24       5       5       0.0154         2       0.9502       17       15       4       4       0.9538       0.0165         1       0.9469       33       31       6       6       0.9574       0.0201         1       0.9452       33       30       6       6       0.9519       0.0152         1       0.9452       33       31       6       6       0.9519       0.0152         1       <	2	0.9670	12	11	3	3	0.9612	0.0129	
2       0.9620       13       10       3       3       0.9582       0.0196         2       0.9603       33       18       6       4       0.9580       0.0196         2       0.9566       35       33       6       6       0.9570       0.0154         2       0.9570       30       14       6       4       0.9570       0.0154         2       0.9553       31       16       6       4       0.9553       0.0165         2       0.9550       27       24       5       5       0.9553       0.0154         2       0.9519       20       14       4       4       0.9538       0.0165         2       0.9502       17       15       4       4       0.9536       0.0184         1       0.9469       33       31       6       6       0.9579       0.0165         1       0.9452       33       30       6       6       0.9519       0.0162         1       0.9452       33       31       6       0.9577       0.0181         1       0.9435       31       29       6       6       0.9577       0.0181 <th>2</th> <th>0.9654</th> <th>35</th> <th>18</th> <th>6</th> <th>4</th> <th>0.9593</th> <th>0.0169</th> <th></th>	2	0.9654	35	18	6	4	0.9593	0.0169	
2       0.9620       13       10       3       3       0.9582       0.0164         2       0.9603       33       18       6       4       0.9580       0.0196         2       0.9566       35       33       6       6       0.9570       0.0154         2       0.9570       30       14       6       4       0.9570       0.0154         2       0.9553       31       16       6       4       0.9553       0.0165         2       0.9550       27       24       5       5       0.9553       0.0154         2       0.9519       20       14       4       4       0.9538       0.0165         2       0.9502       17       15       4       4       0.9536       0.0184         1       0.9459       33       31       6       6       0.9574       0.0201         1       0.9452       33       30       6       6       0.9519       0.0152         1       0.9435       31       29       6       6       0.9519       0.0181         1       0.9435       31       29       6       6       0.9510	2	0.9637	8	2	3	1	0.9587	0.0160	GH30 and GH35 come
2       0.9586       35       33       6       6       0.9579       0.0154         2       0.9570       30       14       6       4       0.9570       0.0154         2       0.9553       31       16       6       4       0.9570       0.0154         2       0.9536       27       24       5       5       0.9553       0.0154         2       0.9519       20       14       4       4       0.9538       0.0165         2       0.9502       17       15       4       4       0.9536       0.0184         1       0.9468       10       2       3       1       0.9534       0.0208         1       0.9452       33       30       6       6       0.9519       0.0152         1       0.9452       33       30       6       6       0.9519       0.0161         1       0.9452       33       30       6       6       0.9519       0.0162         1       0.9435       31       29       6       6       0.9510       0.0181         1       0.9402       35       16       6       4       0.9503	2	0.9620		10	3	3	0.9582	0.0160	drise and driss come
2       0.9570       30       14       6       0.9570       0.0159         2       0.9553       31       16       6       4       0.9565       0.00159         2       0.9553       31       16       6       4       0.9565       0.0159         2       0.9553       31       16       6       4       0.9563       0.0154         2       0.9502       17       15       4       4       0.9534       0.0201         1       0.9459       23       31       6       6       0.9519       0.0165         1       0.9452       33       30       6       6       0.9519       0.0162         1       0.9452       33       6       6       0.9519       0.0162         1       0.9452       33       16       6       0.9519       0.0162         1       0.9452       33       10       0.9507       0.0181       0.0201         1       0.9402       33       16       6       0.9507       0.0181       0.0146	2	0.9603	33	18	6	4	0.9580	0.0196	from samo E2
2       0.9553       31       16       6       4       0.9555       0.0099         2       0.9536       27       24       5       5       0.9553       0.0154         2       0.9536       27       24       5       5       0.9553       0.0154         2       0.9536       27       24       5       5       0.9553       0.0154         2       0.9506       17       15       4       4       0.9538       0.0185         2       0.9466       10       2       3       1       0.9534       0.0208         1       0.9469       33       31       6       6       0.9519       0.0152         1       0.9435       31       29       6       6       0.9511       0.0208         1       0.9435       31       29       6       6       0.9511       0.0208         1       0.9435       31       29       6       6       0.9511       0.0208         1       0.9402       35       16       6       4       0.9503       0.0146	2	0.9586	35	33	6	6	0.9579	0.0154	ITUIT Same FS
2       0.9536       27       24       5       5       0.9553       0.0154         2       0.9519       20       14       4       4       0.9538       0.0164         2       0.9502       17       15       4       4       0.9536       0.0185         1       0.9469       33       31       6       6       0.9519       0.0208         1       0.9469       33       31       6       6       0.9519       0.0161         1       0.9452       33       30       6       6       0.9519       0.0152         1       0.9435       31       29       6       6       0.9510       0.0181         1       0.9435       31       29       6       6       0.9510       0.0181         1       0.9402       35       16       6       4       0.9503       0.0146		0.9570		14	6	4	0.9570	0.0159	
2       0.9519       20       14       4       4       0.9538       0.0165         2       0.9502       17       15       4       4       0.9536       0.0185         1       0.9469       10       2       3       1       0.9534       0.0208         1       0.9469       33       31       6       6       0.9524       0.0201         1       0.9469       33       31       6       6       0.9519       0.0152         1       0.9435       31       29       6       6       0.9510       0.0181         1       0.9435       31       29       6       6       0.9510       0.0181         1       0.9402       35       16       6       4       0.9503       0.0146		0.9553	31	16	6	4	0.9565	0.0099	
2       0.9519       20       14       4       4       0.9538       0.0165         2       0.9502       17       15       4       4       0.9536       0.0185         1       0.9469       10       2       3       1       0.9534       0.0208         1       0.9469       33       31       6       6       0.9519       0.0181         1       0.9452       33       30       6       6       0.9519       0.0152         1       0.9435       31       29       6       6       0.9510       0.0181         1       0.9402       35       16       6       4       0.9503       0.0146	2	0.9536	27	24	5	5	0.9553	0.0154	GH27 is from a cross
1       0.9486       10       2       3       1       0.9534       0.0208         1       0.9469       33       31       6       6       0.9524       0.0201         1       0.9452       33       30       6       6       0.9519       0.0152         1       0.9435       31       29       6       6       0.9511       0.0208         1       0.9435       31       29       6       6       0.9511       0.0208         1       0.9402       35       16       6       4       0.9503       0.0181					4	4			
1         0.9469         33         31         6         6         0.9524         0.0201           1         0.9452         33         30         6         6         0.9524         0.0201           1         0.9452         33         30         6         6         0.9519         0.0152           1         0.9435         31         29         6         6         0.9511         0.0201           1         0.9418         12         3         3         1         0.9507         0.0181           1         0.9402         35         16         6         4         0.9503         0.0146			17	15		4			involving GH25
1         0.9452         33         30         6         6         0.9519         0.0152           1         0.9435         31         29         6         6         0.9511         0.0208           1         0.9418         12         3         3         1         0.9507         0.0181           1         0.9402         35         16         6         4         0.9503         0.0146				-	3				
1         0.9435         31         29         6         6         0.9511         0.0208           1         0.9418         12         3         3         1         0.9507         0.0181           1         0.9402         35         16         6         4         0.9503         0.0146					-	-			
1         0.9418         12         3         3         1         0.9507         0.0181           1         0.9402         35         16         6         4         0.9503         0.0146					-	-			
<b>(15F)</b> 1 0.9402 35 16 6 4 0.9503 0.0146					-	-			
					-				
	designation 1	0.9385	30	16	6	4	0.9501	0.0161	

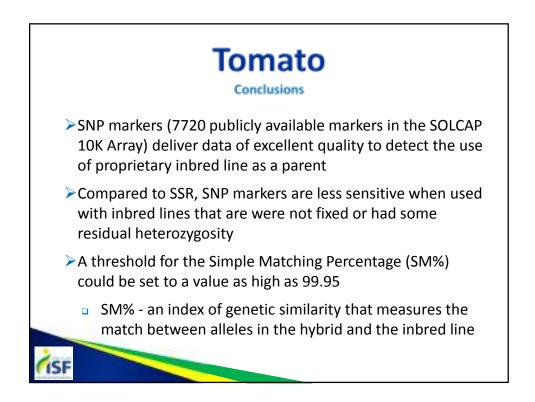






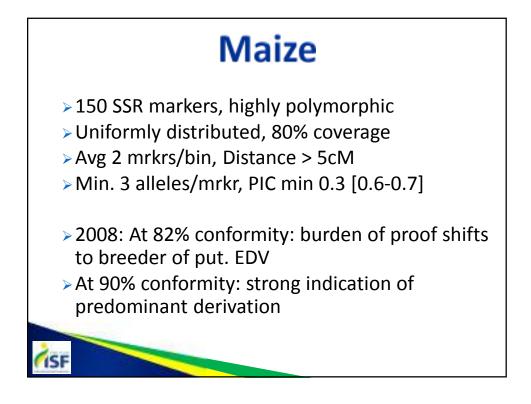


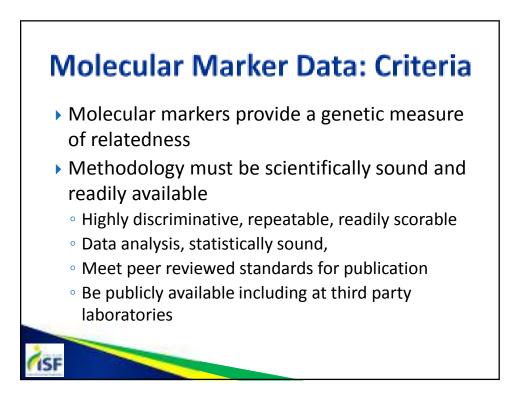


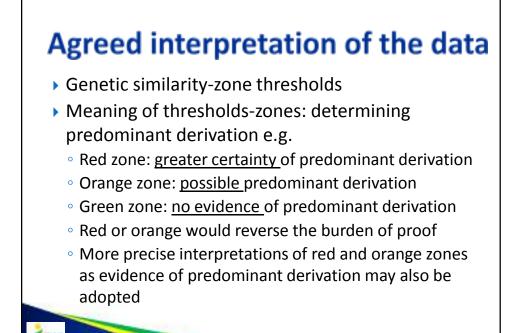








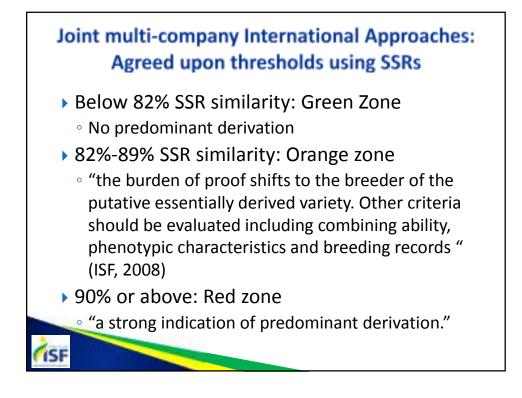


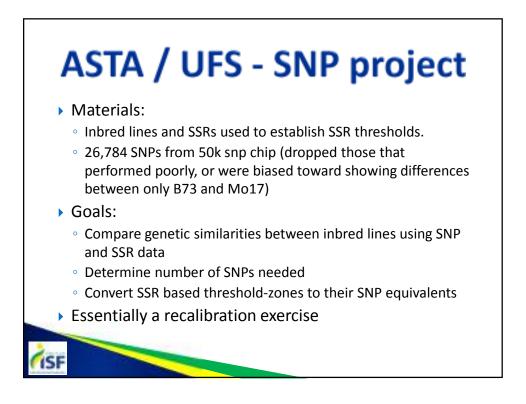


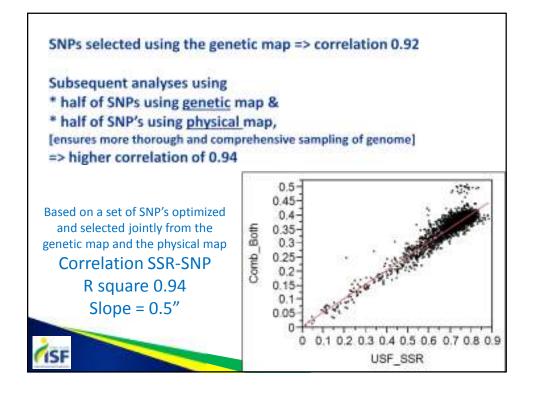
## Joint multi-company International Approaches: SSRs

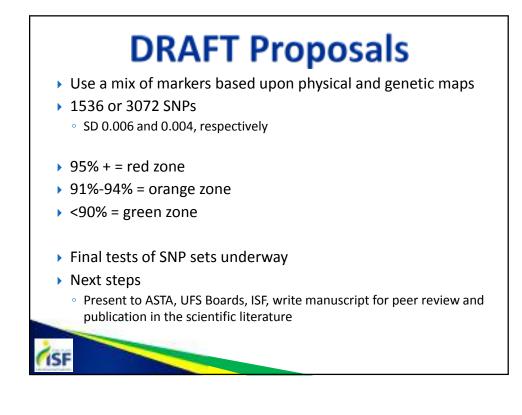
 Early 2000s, ASTA, SEPROMA, and experts from Germany (Univ. of Hohenheim) examined SSR data:

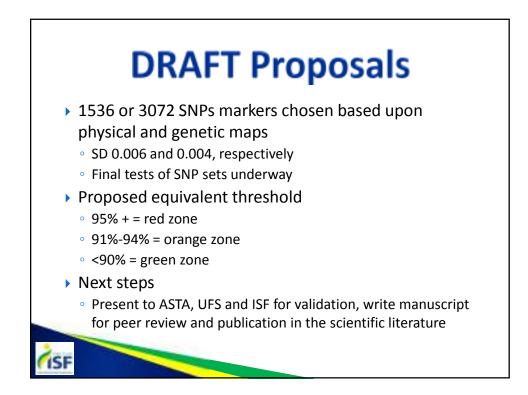
- 1) US inbreds of known pedigree (unrelated-99% similar)
- 2) Inbreds PVP'd in Europe of (largely) unknown pedigree, but of known performance
- 3) computer modeling simulation studies

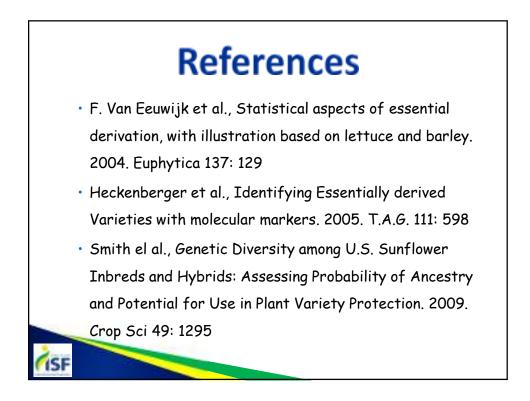




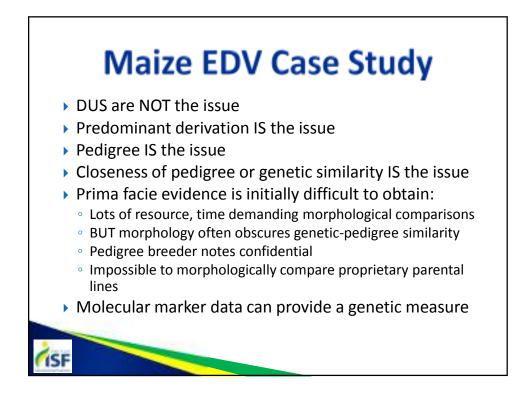










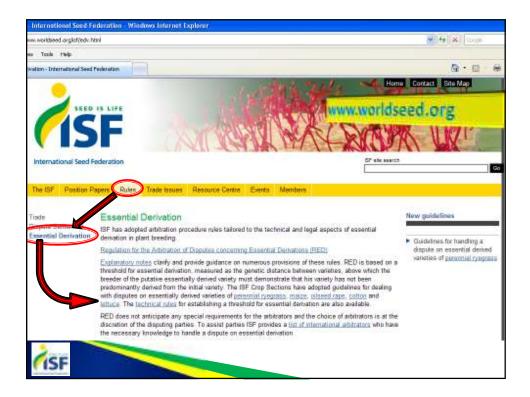


## ASTA / UFS - SNP project

- SNPs replacing SSRs
- Scientific team

ISF

- Post-doc Yves Rousselle
- INRA Plant Genetics group, Alain Charcosset, France
- Rex Bernardo Univ Minnesota USA
- Benjamin Stich Max Planck Institute Germany
- ASTA and UFS company representatives
  - Agreliant, Caussade Semences, Dow, Euralis, KWS, Limagrain, Maïsadour, Monsanto, DuPont Pioneer, RAGT, Syngenta,



## 22/10/2013

